APPENDIX H

SURF OBSERVATION REPORT (SUROB)

SURF OBSERVATION REPORT (SUROB) AND INSTRUCTIONS

1. <u>Line Alpha</u>. Line Alpha is the significant breaker height, or the average height of the highest one-third of all the waves observed during the report. Only the thirty-three (33) highest waves will be used to determine the significant breaker height. The significant wave height is recorded to the nearest one-half foot.

2. <u>Line Bravo</u>. The maximum breaker height, or highest recorded breaker, recorded to the nearest one-half foot.

3. <u>Line Charlie</u>. The breaker period, or average time interval in seconds between breakers observed in Line Alpha. Done by recording time began, to the last breaker counted, and dividing by one-hundred (100), or number of breakers recorded.

4. <u>Line Delta</u>. The percentage of various breaker types. Recorded using the worksheet circling "S" for spilling, "P" for plunging, or "X" for surging, the divided by one-hundred (100) to determine percentage for each.

a. <u>Spilling Breakers</u>. Characterized by the top portion of the breaker becoming unstable at various points and forming foam, which then spills and expands down the front of the breaker in a mild action.

b. <u>Plunging Breakers</u>. Characterized by the top portion of the breaker becoming unstable along the entire frontage very quickly, crashing over itself with a violent release of energy.

c. <u>Surging Breakers</u>. Characterized by appearing as a combination of spilling and plunging breakers. Initially the breaker takes on the characteristics of a plunging breaker, and suddenly changes to appear as a spilling breaker. These occur mostly on steep gradients.

5. <u>Line Echo</u>. The breaker angle, or the orientation of the breaker frontage in relation to shore. Done by calculating the acute angle formed between the breaker lines and the shoreline, and expressed in five (5) degree increments towards either right (R) or left (L) flank as the observer faces towards land from the seaward.

6. <u>Line Foxtrot</u>. The littoral current, or speed in knots of the water flowing parallel to the shore just inside the main line of breakers. Calculated by throwing an object into the surf zone as far as possible, and observing the distance (in feet) to which the object travels for one (1) minute. The number of feet travelled is then divided one-hundred (100) to determine speed in knots. Recorded to the nearest tenth of a knot and towards which flank (R or L) the object travelled.

7. <u>Line Golf</u>. Concerns two pieces of information; the Depth of the Surf Zone, and Lines of Breakers present therein. The lines of breakers are determined by counting the number of well-defined breaker lines. Depth (distance) is conducted by estimating the distance from the outermost breaker line to the furthest limit of the up-rush of water on shore.

8. <u>Line Hotel</u>. Covers several miscellaneous items of information, to be passed in plain text:

Updated Surf Observation (SUROB) Report

SURF OBSERVATION REPORT (SUROB) FORMAT

NAME & RANK OF OBSERVER: ______ DATE: _____ TIME: _____ BEACH: _____ UNIT: _____

NOTE: BEFORE YOU START RECORDING WAVES YOU MUST REFER TO THE SUROB WORKSHEET PROVIDED. BEGIN BY STARTING YOUR STOPWATCH. WHILE OBSERVING EACH OF THE 100 WAVES, MAKE NOTE OF THE TYPE (P=PLUNGING, S=SPILLING OR X=SURGING) OF WAVES AND RECORD IT AS APPROPRIATE. ONCE THE 100TH WAVE IS OBSERVED, STOP THE STOPWATCH

LINE		INFORMATION								SUR	OB I	DAT	4	MS	SI	NOTES:											
Α	SIGNIFICANT BREAKER HEIGHT IN FEET.							г.	FEET=						OB TH AL EX	OBSERVE 100 WAVES. ONLY THE HIGHEST 33 WAVES WILL BE ADDED TOGETHER ANI THEN DIVIDED BY 33 FOR THE SIGNIFICANT BREAKER HEIGHT. THE MSI FACTOR WIL ALWAYS BE THE SAME AS THE BREAKER HEIGHT WITH A DECIMAL POINT ADDED. EXAMPLE: 3 FEET = 3.0 MSI THE IS THE SINCLE HICHEST WAVE OPERFYED DURING THE 100 WAVE COUNT. MOL								ND TLL			
B	B MAXIMUM BREAKER HEIGHT IN FEET.								FEET N/A THIS IS THE SINGLE HIGHEST WAVE OBSERVED DURING THE 100 WAVE NOT COMPUTED IN THIS LINE.						AVECC	UNT. MS	IIS										
C BREAKER PERIOD IN SECONDS.								SEC					N SECON AVES. E /ES = 13	DS THA' XAMPLE .2 SECO	T WAS R 5: 22 MII NDS. US	ECORDE N = 1320 SE THE	D										
									BR	EAKE	R PER	IOD	MODIFIC	CATIO	N TAB	LE	-	-									
									1	17 (0.0	-0.1	-0.2	-0.3	-0.4	-0.5	-0.6	-0.8	-1.0	_							ľ
											0.0	-0.1	-0.1	-0.2	-0.2	-0.3	-0.4	-0.5	-0.8	_							
							в	REAKE	R 1			0.0	-0.1	-0.1	-0.1	-0.2	-0.2	-0.3	-0.3								
							1	PERIOD		13 ().0	0.0	0.1	0.0	0.0	0.0	0.0	0.3	0.3								
								IN	1	12 0	0.0	0.1	0.1	0.2	0.2	0.3	0.4	0.5	0.7								
							S	ECOND	s 1	1 0).0	0.1	0.2	0.3	0.4	0.5	0.6	0.8	1.0								
									1	10 0).1	0.1	0.2	0.3	0.5	0.7	0.9	1.1	1.3								
						90).1	0.1	0.3	0.3	0.6	0.8	1.1	1.3	1.7												
	-						8 (0.1	0.2	0.3	0.3	0.7	1.0	1.3	1.6	2.0											
								J	 ST	1.5 CNIFI	2.0 CAN	2.5 T BREAK	3.0 (FR HI	J.5 FICHT	4.0	4.5 T	5.0										
DDEAKED TVDEC.									51	011111	CAL	I DREAN		AS	EACH	VAVE IS	OBSERV	ED IT IS	RECORI	DED ON '	THE SUF	ROB WOI	RKSHEE	Т.			
	DALAREN I II EO.								0/	PI I	NGIN	G			P=	PLUNGI	NG S=SP	ILLING	X=SUR	GING DI	VIDE TH	E NUME	BER OF E	ACH BE	EAKER 1	YPE	
D	DI 1	UNG	ING 9	SDILT I	NGO	R SIII	RGING	Ţ		% SPILLING BY 100. THIS WILL GIVE YOU PERCENTAG							LUE T	E OF EAC	TH BREA	TABLE F	PE. REF. FOR PLU	ER TO TH NGING	E				
		01101	ino, i		100	K SUI	NOINC	J		% SURGING WAVES. <u>YOU WILL ONLY RECORD THE LOWEST MSI VALUE FROM EITHER</u>							HER										
							DIT								DMOD	TELCA											
		100		ING BE	CEAKE				ABLE	2.2	41	5.0				100		AING B	0 5				ABLE	3.2	41	50	
	F	90	0.0	-0.2	-0.4	-0.7	-1.5	-1.6	-2.2	-2.9	-3.6	-3.0			ŀ	90	0.0	0.2	0.4	0.8	1.3	1.7	2.3	3.0	3.8	4.7	
	F	80	0.0	-0.2	-0.4	-0.6	-1.0	-1.4	-2.0	-2.6	-3.2	-4.0)		F	80	0.0	0.2	0.4	0.7	1.1	1.6	2.2	2.9	3.6	4.5	
	Ē	70	0.0	-0.1	-0.3	-0.6	-0.9	-1.3	-1.7	-2.2	-2.8	-3.5	;		-	70	0.0	0.2	0.4	0.6	1.0	1.5	2.0	2.7	3.4	4.2	
PERCE	INT	60	0.0	-0.1	-0.2	-0.5	-0.8	-1.1	-1.5	-1.9	-2.4	-3.0)	PERCE	ENT	60	0.0	0.2	0.3	0.6	1.0	1.4	1.9	2.5	3.1	3.9	
SPILLI BDFAK	NG FDS	50	0.0	-0.1	-0.2	-0.4	-0.6	-0.9	-1.2	-1.6	-2.0	-2.5	;	SUKGI	NG FDS	50	0.0	0.1	0.3	0.6	0.9	1.3	1.7	2.3	2.9	3.5	
DREAK	ERS	40	0.0	-0.1	-0.2	-0.3	-0.5	-0.7	-1.0	-1.3	-1.6	-2.0	<u> </u>	DREAK	LINS	40	0.0	0.1	0.3	0.5	0.8	1.1	1.5	2.0	2.6	3.2	
	-	20	0.0	-0.1	-0.1	-0.2	-0.4	-0.5	-0.7	-1.0	-1.2	-1.5	-		-	20	0.0	0.1	0.2	0.4	0.7	1.0	1.3	1.ð 1.4	2.2 1.8	2.7	
	ŀ	10	0.0	0.0	0.0	-0.2	-0.3	-0.4	-0.2	-0.3	-0.4	-0.5			-	10	0.0	0.1	0.2	0.3	0.4	0.6	0.7	1.9	1.3	1.6	
	F	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-			0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	-		0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0					0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	
		SIGNIFICANT BREAKER HEIGHT IN FEE								TEET								SIG	NIFICA	NT BR	EAKER	HEIGH	IT IN F	EET			

LINE	INFORMATION								SUROB DATA				MSI		NOTES	5:						
E	BREAKER ANGLE: IN DEGREES TOWARD									o					THIS IS THE ANGLE WAVES BREAK ON THE SHORE. AND IT IS MEASURED IN							
	THE RIGHT OR LEFT FLANK.								RIGH	IT/LEF	T			:	DEGREES. I MODIFICAT	N N ION	AOST CASES I TABLE BEI	TT WILL NOT EX	CEEI SI FA	D 5 DEGREES	5. USE THE T OF LEFT FLAN	IK
									FL	ANK			•		IS DETERMINED AS IF YOU WERE LANDING ON THE BEACH.							
	WAVE ANGLE MODIFICATION TABLE														LITTOR	٩L	CURRENT	MODIFICATI	ON '	TABLE		
	40 0.1 0.3 0.7 1.3 2.0 2.9 3.							3.9	5.1	6.5	8.0]	KNOTS	MS	I MOD		KNOTS	MSI MOD		KNOTS	MSI MOD	
	35	0.1	0.3	0.6	1.1	1.8	2.5	3.4	4.5	5.7	7.0		0.0=	0.0			1.0=	3.0]	2.0=	6.0	
	30	0.1	0.2	0.5	1.0	1.5	2.2	2.9	3.8	4.9	6.0		0.1=	0.3			1.1=	3.3		2.1=	6.3	
WAVE	25	0.1	0.2	0.5	0.8	1.3	1.8	2.5	3.2	4.1	5.0		0.2=	0.6			1.2=	3.6		2.2=	6.6	-
ANGLE IN DECREES	20	0.0	0.2	0.4	0.6	1.0	1.4	2.0	2.6	3.2	4.0	┨ _	0.3=	0.9			1.3=	3.9	4	2.3=	6.9	-
DEGREES	15	0.0	0.1	0.3	0.5	0.8	1.1	1.5	1.9	2.4	3.0	┨	0.4=	1.2			1.4=	4.2	4	2.4=	7.2	-
	10	0.0	0.1	0.2	0.3	0.5	0.7	1.0	1.3	1.6	2.0	┨	0.5=	1.5			1.5=	4.5	4	2.5=	7.5	-
	5	0.0	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.8	1.0	┨	0.6=	1.8			1.6=	4.8	-	2.6=	7.8	-
	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4	0.7=	2.1			1.7=	5.1		2.7=	8.1	-
		0.5			2.0	2.5	3.0	3.5	4.0 FFT	4.5	5.0	+ -	0.8=	2.4			1.8=	5.4	$\left\{ \right.$	2.8=	8.4	
			516	INIFICA	INI BK	EAKEK	HEIGH	11 IN F.	EEI			┦└	0.9=	2.1			1.9=	5./		2.9=	8./]
		DAT 4	יםסודי	ENT.						KNO	тс			—	THROW A B	UO	YANT OBJEC	CT INTO THE WA	TER	AND BEGIN	TIMING ONE	
					DICU				DICI	<u> </u>					MINUTE. PACE OFF THE DISTANCE THE OBJECT TRAVELED IN FEET OV							ΉE
F	IN KING	KNOTS TOWARD THE RIGHT OR LEFT				RIGH1/LEF1				•		PERIOD OF ONE MINUTE. NOW DIVIDE THE DISTANCE THE OBJECT TRAVELED										
L '	FLANK									LANK				BY 100. EXA MSI FACTOR	AMI >	PLE: 80 FEET	TRAVELED $= 0.8$	3 KNO	OTS USE TA	BLE ABOVE FOR		
	SUDE ZONE								LINES						COUNT THE NUMBER OF SWELLS & BREAKERS WITHIN YOUR SPLASH AREA,							
													N/A		THIS IS THE NUMBER FOR "LINES OF BREAKERS". DEPTH IS MEASURED FROM							ЭM
G	LINES OF BREAKERS &							FFF					THE CLOSEST BREAKING WAVE TO THE FURTHEST APPROACHING SWELL & IS									
0	DEPTH OF SUKF ZONE IN FEET							_FEEI					DONE SO IN	FE	EL NO MSI I	FACTOR IS USED			AC METHOD			
	ADDITIONAL REMARKS:									_KNO	TS				WIND SPEEI	515	MEASUREL	IN KNOTS USIN	GIH	IE KANGE FL	AG METHOD.	
	WIND	SPEED	D/DIRE	CTION	<u>N</u> : IN			_	0						WIND DIREC	CTI	ON IS MEAS	URED IN DEGREE	ES TO	WARD THE	RIGHT OR LEFT	
	KNOTS	S/DEG	REES 1	ГОWA	RDS T	THE		F	RIGHT/LEFT FLANK				•		FLANK TO THE BEACH. IF THE WIND IS BLOWING ONTO THE BEACH IT IS							
H	RIGHT	/LEFT	FLAN	K				F							"ONSHORE"	WI	IND. IF THE	WIND IS BLOWIN	NG O	NTO THE OC	EAN IT IS	
	WIND:	ONSE	IORE (OR OF	FSHO	RE(CIR	CLE ON	JE)							OFFSHORE	vv	IND.					
		-	-			X -		. ,			ODIEL											
	WIND MOD									E WIN	D	TABLE	OF	FSHORE W	INT)						
							3	36-40	2.0	3	.0	4.0		1.	5 2.0		4.0					
						WIND	3	31-35	1.5	2	.0	3.0		1.	0 1.5		3.0					
						SPEEL	2	26-30	1.0	1	.5	2.0		0.	5 1.0		2.0					
						KNOTS	3 4	6 20	0.5	1	.0	1.5		0.	0 0.5		1.5					
							1	1-15	0.0	0	.0	0.5		0.	0 0.0	_	1.0					
								6-10	0.0	0	.0	0.5		0.	0 0.0		0.5					
								0-5	0.0	0	.0	0.0		0.	0 0.0		0.0					
					_				0-30	30	-60	60-90		0-3	30 <u>30-60</u>		60-90					
	SECON		7 337 A 37		CUT		T			V	VIND A	NGLE R	ELATIVE 1		E BEACH SECONDAR	Y W	AVE HEIGH	T REFERS TO AN		DITIONAL SI	REZONE BEVON	ND
	SECON	IDAK 1	WAV	E HEI	<u>GHI</u> :	IN FEE	51								THE INITIAL	su	JRF ZONE OI	R ONE APPROAC	HINC	A DIFFERE	NT ANGLE. THIS	5
TT										FEE	Γ.		•		WILL USUALLY OCCUR ONLY ON BEACHES WITH A REEF EXTENDING							
H															BEYOND TH	IE II	NITIAL SURI	F ZONE AND IS R	ARE	LY ENCOUN	FERED. THE MSI	I IS
(CONT)	DEDDI			ONE · (CENIE		ESCD	DTIO		DIECT	rc	<u> </u>			GENER AT		SCRIPTION	JOFANY ORIE	CTS	IN THE SU	RE ZONE	
	DERKI	5 111 5	SUKF ZUNE: GENERAL DESCRIPTION OF OBJECTS							13.		N/A		EXAMPLE	U U	OGS. FISHI	NG NETS			NI ZONE.		
				~ · -								ļ'			DD.							
	SEE ST	ATE:		CAI	_M / N	10DER	ATE /	ROUC	Η				N/A									
	(CIRCLE ONE)									-												

TIN	AE BEGA	AN:		_MIN.		SI	EC.				
	1	2	3	4	5	6	7	8	9	10	TOTAL NUMBER OF
1											PLUNGING = \div 100= %
	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	
2											TOTAL NUMBER OF
	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	TOTAL NOWIDER OF
3						D.G. W					SPILLING= $_$ 100= %
	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	
4											TOTAL NUMBER OF
5	PSX	PSX	PSX	PSX	PSX	PSX	PSX	PSX	PSX	PSX	SUPCING- \div 100- %
3	DS V			DS V	DS V	DS V	DS V		DS V		SUKUINU 100- %
6	гэл	гэл	гэл	гэл	гэл	гэл	гэл	гэл	гэл	гэл	TOTAL TIME IN GECONDS TO
0	$\overline{PS X}$	$\overline{PS X}$	$\overline{PS X}$	\overline{PSX}	TOTAL TIME IN SECONDS TO						
7	IDA	15 /	15 /	15 /	IDA	IDA	IJA	157	IDA	15 /	OBSERVE 100 WAVES=÷
,	\overline{PSX}	\overline{PSX}	\overline{PSX}	\overline{PSX}	\overline{PSX}	\overline{PSX}	\overline{PSX}	\overline{PSX}	\overline{PSX}	\overline{PSX}	100 WAVES= BREAKER PERIOD
8		- ~	- ~							- ~	
	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	
9											
	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	
10											
	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	PS X	
TIM	E ENDE	D:		MIN		S	SEC.				

				SUROB	MSI	INSTRUCTIONS
SIGNIFICAN	T BR	EAKER HEIGHT	COMPUTATION	LINE	FACTOR	
(H	IGHE	EST 33 WAVES OBSE	ERVED)	А		ADD SUROB LINES A, C, & D
WAVE HEIGHT	X	OCCURRENCE	=PRODUCT	В	N/A	TOGETHER. NOW YOU WILL
	X			С		DETERMINE WHICH OF THE TWO
	Х			D		LINES E OR F HAS <u>THE LARGER</u> MSI
	Χ			Е		VALUE AND ADD IT. NOW FINALLY
	Χ			OR		ADD LINES F AND H AND YOU WILL
	Х			F		HAVE YOUR TOTAL MSI FACTOR.
	Х			G	N/A	
TOTAL PRODUC	ст -	-33 = SIGNIFICA	ANT WAVE HEIGHT	Н		A+C+D+ E OR F+H= MSI TOTAL
	~ .			TOTAL		

SEA	STA	ATE CONDITIONS
1		WIND SPEEDS BETWEEN 5 TO 9 MILES PER HOUR (5 TO 8 KNOTS).
		WAVE HEIGHTS CONSIDERED SMALL WAVELETS BETWEEN 0.5 AND 1 FEET (0.6093 TO 0.304 METERS.
		SMALL WAVELETS WITH GLASSY-APPEARING CRESTS AND NO BREAKING.
2		WIND SPEEDS BETWEEN 10 TO 11 MILES PER HOURS (9 TO 10 KNOTS).
		WAVE HEIGHTS CONSIDERED LARGE WAVELETS, BETWEEN 1.5 AND 2 FEET (0.456 TO 0.609 METERS).
		LARGE WAVELETS, CRESTS BEGIN TO BREAK AND WHITECAPS ARE SCATTERED
3		WIND SPEEDS BETWEEN 16 TO 17 MILES PER HOUR (14 TO 15 KNOTS).
		WAVE HEIGHTS CONSIDERED SMALL, BETWEEN 3.5 AND 4 FEET (1.06 TO 1.21 METERS).
		SMALL WAVES BECOMING LONGER AND WHITECAPS ARE NUMEROUS
4		WIND SPEEDS BETWEEN 19 TO 24 MILES PER HOUR (17 TO 21 KNOTS).
		WAVE HEIGHTS CONSIDERED MODERATE, BETWEEN 4 AND 7.5 FEET (1.24-2.5 METERS).
		MODERATE WAVES FORMING NUMEROUS WHITE CAPS AND SOME SPRAY
5		WIND SPEEDS BETWEEN 24 TO 28 MILES PER HOUR (21 TO 25 KNOTS).
		WAVE HEIGHTS CONSIDERED LARGE, BETWEEN 8 AND 12 FEET (2.43 TO 3.65 METERS).
		LARGE WAVES FORM AND WHITECAPS ARE COMMON, ALONG WITH MORE SPRAY.

APPENDIX I

MODIFIED SURF INDEX (MSI) INSTRUCTIONS

1. Modified Surf Index (MSI). The MSI is a single dimensionless number which provides a relative measure of the conditions likely to be encountered in the surf zone. It provides a guide for judging the feasibility of conducting landing operations for each type of landing craft. It is a guide, not definite go or no go criteria. When applied to a known or forecasted surf condition, the MSI calculation provides the commander with an objective method of arriving at a safe and reasonable decision with respect to committing landing craft and amphibious vehicles.

a. Line Alpha (Significant Breaker Height). Refers to Line A of the SUROB and determines the significant breaker height factor. This number is transferred directly over from the SUROB, and is not modified by any table. (A significant breaker height of 3.0 feet converts to a MSI factor of 3.0)

b. Line Charlie (Breaker Period). Refers to Line C of the SUROB. Determined by using the "Breaker Period Modification Table".

c. Line Delta (Breaker Types). Refers to Line D of the SUROB. Record the percentages of the types of breakers that occur rounded to the nearest tenth. There is no modification table for plunging breakers. Record the lower of the two numbers under the MSI factor column.

d. Line Echo (Breaker Angle). Refers to Line E of the SUROB, and determines the breaker angle or the angle of breaker makes with the shoreline. To calculate, transfer data from the SUROB, rounding to the nearest fifth, using the "Wave Angle Modification Table" to determine the MSI factor.

e. Line Foxtrot (Littoral Current). Refers to Line F of the SUROB. Littoral current is one of the most crucial factors in conducting the MSI, because it can severely elevate the overall MSI factor if inaccurate data is submitted. Determine MSI factor by converting data from "Littoral Current Modification Table".

f. Line Hotel (General Data). Refers to Line H of SUROB.

(1) Relative Wind. Transfer respective data from SUROB and use "Wind Modification Table" to determine MSI factor.

(2) Secondary Wave Height. If another series of breakers exists further out past the main series of breakers, then the maximum

height for that system is recorded. The SUROB data is transferred directly to the MSI factor.

g. Total MSI. To get the total MSI factor add lines A through D, the highest of Line E or F, and Line H. The maximum safe MSI as per COMNAVSURFPACINST/COMNAVSURFLANTINST 3840.1B Joint Surf Manual is 6.0.

2. Problems with MSI. Relatively minimal surf conditions can combine to make landing conditions unfeasible. It is important to remember that the MSI is a guide for judging the feasibility of landing operations. MSI tables often do not go high or low enough to calculate some wave conditions, additionally; tables were designed with conventional landing craft in mind. AAVs do not have the exact characteristics as conventional landing craft and often have traction well out in the surf zone. As such, AAVs are not as affected by littoral current and can often negotiate such conditions. Vehicle mechanical factors should be seriously considered, however, the final judgment should come from the AA Unit Commander with eyes on the actual surf conditions. In the absence of direct observation, all factors should be considered when planning a landing with a high MSI.